

Time integration

DVI and HHT time stepping methods in Chrono





Time Integration in Chrono



- Two classes of time stepping methods in Chrono
 - Time steppers for smooth dynamics
 - Classical multibody dynamics rigid and flexible connected through joints
 - FEA
 - Fluid solid interaction problems
 - Time steppers for non-smooth dynamics
 - Scenarios w/ friction and contact

Time Integration – Smooth Dynamics



- Smooth dynamics:
 - Equations of Motion: formulated as Differential Algebraic Equations (DAE)
 - Time-stepping methods:
 - HHT
 - Euler implicit
 - Euler semi-implicit linearized
 - Newmark
 - Require solution of a linear system at each time step
 - MINRES
 - MKL
 - MUMPS, etc.
 - Discontinuous forces if any, are regularized via penalty
 - Can still have friction and contact, but is "smoothed"

Time Integration – Non-smooth Dynamics

- Non-smooth dynamics:
 - Equations of motion formulated as Differential Variational Inequality (DVI) Problems
 - Time-stepping method:
 - Euler implicit linearized (Anitescu-Trinkle)
 - Required solver at each time step: **Cone Complementarity Problem**
 - SOR
 - Barzilai-Borwein
 - APGD
 - Set-valued and discontinuous forces: no need to be "smoothed"
 - •
 - No support for FEA yet







Smooth dynamics - DAE

The HHT Time Stepper

Linear Solvers



Differential problems

• An Ordinary Differential Equation (ODE):

$$\frac{d\boldsymbol{x}}{dt} = \boldsymbol{f}(\boldsymbol{x}, t)$$

- A Differential Algebraic Equation (DAE)
 - In implicit form:

$$\frac{d\boldsymbol{x}}{dt} = \boldsymbol{f}(\boldsymbol{x}, t)$$
$$\boldsymbol{g}(\boldsymbol{x}, t) = \boldsymbol{0}$$

The Chrono case
$$M\frac{dv}{dt}=f(q,v,t)+D_{\mathcal{B}}\widehat{\gamma}_{\mathcal{B}}(t)$$

$$C(q,t)=0$$

• Introduces constraints **g**

DAE Explicit Integrators



• **Explicit** integrators:

$$\boldsymbol{x}(t + \Delta t) = \boldsymbol{F}(\boldsymbol{x}(t))$$

- Very straightforward they do not require solving linear systems
- Require very small time steps, due to stability reasons
- The stiffer the problem, the smaller the time step
- Lead to numerical drift when handling DAEs
- Used by traditional DEM granular dynamics simulators

DAE Implicit Integrators



• Implicit integrators:

$$G(\mathbf{x}(t + \Delta t), \mathbf{x}(t)) = \mathbf{0}$$

- Can use large time steps
- More complex: they find $x(t + \Delta t)$ by solving a nonlinear system G = 0 with Newton Raphson
 - Jacobians matrices of G are needed (ex. stiffness matrices, etc.)
 - Require solution of one or more <u>linear systems</u> at each time step
- Useful both for ODEs and DAEs for the latter, they treat the constraints well
- Used in FEA problems, handle stiffness well

DAE Implicit Integrators in Chrono



- Classical Euler implicit
 - First order accurate, large numerical damping
- Euler semi-implicit linearized (1 step)
 - First order accurate, large numerical damping
 - Same time-stepping used for DVI non-smooth dynamics, it can use complementarity solvers
- Trapezoidal
 - Second order accurate, no numerical damping
 - Doesn't work well with joints (kinematic constraints)
- Newmark
 - Adjustable numerical damping, first order (except in particular case)
- HHT
 - Second order accurate, adjustable numerical damping
 - Most used integrator for FEA problems in Chrono



The HHT integrator

• The DAE problem is:

$$M\frac{dv}{dt} = f(q, v, t) + D_{\mathcal{B}}\widehat{\gamma}_{\mathcal{B}}(t)$$
$$C(q, t) = 0$$

• The HHT time discretization is:

$$q^{l+1} - q^l - hv^l - \frac{h^2}{2} \left[(1 - 2\beta)a^l + 2\beta a^{l+1} \right] = 0$$
$$v^{l+1} - v^l - h \left[(1 - \gamma)a^l + \gamma a^{l+1} \right] = 0$$
$$Ma^{l+1} + (1 + \alpha)(C_q^T \lambda - f)^{l+1} - \alpha(C_q^T \lambda - f)^l = 0$$

- A-stable for: • 2-nd order accurate $\gamma = \frac{1-2\alpha}{2}$ $\beta = \frac{(1-\alpha)^2}{4}$
- An alternative formulation $\alpha \in [-\frac{1}{3}, 0]$ ion-level HH 1 2
- Adjustable parameter α : from 0 (no numerical damping; i.e., trapezoidal) to -1/3 (max numerical damping)

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The HHT integrator

• The $G(x(t+\Delta t), x(t)) = 0$ non-linear problem to solve is:

$$\boldsymbol{q}^{l+1} - \boldsymbol{q}^{l} - h\boldsymbol{v}^{l} - \frac{h^{2}}{2} \left[(1 - 2\beta)\boldsymbol{a}^{l} + 2\beta\boldsymbol{a}^{l+1} \right] = 0$$
$$\boldsymbol{v}^{l+1} - \boldsymbol{v}^{l} - h \left[(1 - \gamma)\boldsymbol{a}^{l} + \gamma \boldsymbol{a}^{l+1} \right] = 0$$
$$M\boldsymbol{a}^{l+1} + (1 + \alpha)(C_{\boldsymbol{q}}^{T}\boldsymbol{\lambda} - \boldsymbol{f})^{l+1} - \alpha(C_{\boldsymbol{q}}^{T}\boldsymbol{\lambda} - \boldsymbol{f})^{l} = 0$$

• Its Newton-Raphson step requires solving this **linear system**:

$$\begin{bmatrix} H & \overline{C}_{q}^{T} \\ \overline{C}_{q} & 0 \end{bmatrix} \left\{ \begin{array}{l} \Delta a^{l+1} \\ \Delta \lambda^{l+1} \end{array} \right\} = \\ \left\{ \begin{array}{l} \frac{1}{1+\alpha} (Ma^{l+1}) + (C_{q}^{T}\lambda - f)^{l+1} - \frac{\alpha}{1+\alpha} (C_{q}^{T}\lambda - f)^{l} \\ \frac{1}{\beta h^{2}} C^{l+1} \end{array} \right\} \\ a^{l+1}_{n+1} = a^{l+1}_{n} + \Delta a^{l+1} \\ \lambda^{l+1}_{n+1} = \lambda^{l+1}_{n} + \Delta \lambda^{l+1} \\ v^{l+1} = v^{l} + h \left[(1-\gamma)a^{l} + \gamma a^{l+1} \right] \\ q^{l+1} = q^{l} + hv^{l} + \frac{h^{2}}{2} \left[(1-2\beta)a^{l} + 2\beta a^{l+1} \right] \\ H = \left[M - \gamma h \nabla_{v} f^{l+1} - \beta h^{2} \nabla_{q} f^{l+1} + \beta h^{2} \left[(Ma)_{q} + (C_{q}^{T}\lambda)_{q} \right] \right]^{11}$$

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Configuring the Integrator in Chrono

- It can be changed with SetTimestepperType()
- Additional parameters via std::static_pointer_cast<...>(my_system.GetTimestepper())

// change the time integration to Euler, also suitable for NSC too (this is the default)
my_system.SetTimestepperType(ChTimestepper::Type::EULER_IMPLICIT_LINEARIZED);

```
// change the time integration to HHT:
my_system.SetTimestepperType(ChTimestepper::Type::HHT);
auto integrator = std::static_pointer_cast<ChTimestepperHHT>(my_system.GetTimestepper());
integrator->SetAlpha(-0.2);
integrator->SetMaxiters(8);
integrator->SetAbsTolerances(5e-05, 1.8e00);
integrator->SetMode(ChTimestepperHHT::POSITION);
integrator->SetModifiedNewton(false);
integrator->SetScaling(true);
integrator->SetVerbose(true);
```



Linear System Solvers

- All DAE solvers require solving a linear system
- Linear system solvers are independent from the time integrator
 - One can mix and match
- Available linear system solvers
 - MINRES (iterative solver, free)
 - MKL (direct solver, requires license)
 - MUMPS (direct solver, free)
- Moving forward:
 - MUMPS with OpenBLAS since they are both free and licensed under BSD



Linear System Solvers: MINRES

- Available in the main Chrono unit
- A Krylov-type iterative solver
- Convergence might slow down when large mass or stiffness ratios are used
- Robust in case of redundant constraints
- Warm starting can be used to reuse last solution (faster solution)

```
// Change solver settings
my_system.SetSolverType(ChSolver::Type::MINRES);
my_system.SetSolverWarmStarting(true);
my_system.SetMaxItersSolverSpeed(200); // Max number of iterations for main solver
my_system.SetMaxItersSolverStab(200); // Used only by few time-integrators
my_system.SetTolForce(1e-13);
```



Linear System Solvers: MKL

- MKL Intel libraries must be licensed and installed on your system,
- Available in the optional Chrono::MKL unit (enable it in Cmake)
- Direct parallel solver: no iterations are needed
- Not robust in case of redundant constraints avoid them!
- Cannot use SetSolverType(), you must create a solver and plug it in the ChSystem:

```
#include "chrono_mkl/ChSolverMKL.h"
...
// change the solver to MKL:
auto mkl_solver = std::make_shared<ChSolverMKL<>>();
my_system.SetSolver(mkl_solver);
mkl_solver->SetSparsityPatternLock(true);
mkl_solver->SetVerbose(true);
```

Linear System Solvers: MUMPS



- Work in progress to be wrapped up by mid January
- Direct parallel solver
- Developed in France/UK, relies on OpenBLAS, which developed in China
- Free solution, source code available for MUMPS & OpenBLAS

```
#include "chrono_mkl/ChSolverMUMPS.h"
...
// change the solver to MUMPS:
auto mumps_solver = std::make_shared<ChSolverMUMPS<>>();
my_system.SetSolver(mumps_solver);
mumps_solver->SetSparsityPatternLock(true);
```



Non-Smooth dynamics - NSC

The DVI time-stepper

The CCP solvers



Variational Inequalities

• Definition of Variational Inequality (VI):

$$\boldsymbol{x} \in \mathbb{K}$$
 : $\langle F(\boldsymbol{x}), \boldsymbol{y} - \boldsymbol{x} \rangle \ge 0 \quad \forall \boldsymbol{y} \in \mathbb{K}$

- for continuous $F({m x}): {\mathbb K} o {\mathbb R}^n$
- with closed and convex \mathbb{K}

(see Kinderleher and Stampacchia ,1980)

•Alternative formulation:

$$\mathbf{x} \in \mathscr{K}, \ \mathbf{g}(\mathbf{x}) \in -\mathsf{N}_{\mathscr{K}}(\mathbf{x})$$
$$\mathsf{N}_{\mathscr{K}}(\mathbf{x}) = \{\mathbf{y} \in \mathbb{R}^{n} : \langle \mathbf{y}, \mathbf{x} - \mathbf{z} \rangle \ge 0, \forall \mathbf{z} \in \mathscr{K}\}$$



Differential Variational Inequality



• Differential Variational Inequality (DVI)

$$\begin{aligned} \frac{d\boldsymbol{x}}{dt} &= f(t, \boldsymbol{x}, \boldsymbol{u}) \\ \boldsymbol{u} \in \text{SOL}\left(\mathbb{K}, F(t, \boldsymbol{x}(t), \cdot)\right) \\ \Xi(\boldsymbol{x}(0), \boldsymbol{x}(T)) &= 0 \end{aligned}$$

where $\mathsf{SOL}\left(\mathbb{K}, F(t, \bm{x}(t), \cdot)\right)$ is the set of solutions to the VI $(\mathbb{K}, F(t, \bm{x}(t), \cdot))$

• It is also a special class of Differential Inclusion (DI), $dx/dt \in f(x,t)$

Differential Inclusions: motivation

• Most differential problems can be posed as equalities like:

dx/dt = f(x,t) \rightarrow ODE, DAE, ok

• But some problems require inequalities or inclusions like

 $dx/dt \in f(x,t)$ \rightarrow Differential Inclusion! (DI)

• Example: a flywheel with brake torque and applied torque (looks simple?!)

•
$$J \, d\omega/dt = M_f(\omega) + M_e(t)$$
 where $M_f = -M_{fmax}$ if $\omega > 0$
and $M_f = M_{fmax}$ if $\omega < 0$

- All ODE integrator would never stop in $\omega = 0$! It would just ripple about $\omega = 0$..
- Reducing Δt in ODE integrator may reduce the ripple, But what if low J ? Divergence!
- Regularization methods? A) Numerical stiffness!
 B) Approximation! C) The brake would never stick! ...
- Also, if ever $\omega = 0$, which M_f ? Not computable!









Differential Inclusions: motivation

- Most differential problems can be posed as equalities like:
 - dx/dt = f(x,t) \rightarrow ODE, DAE, ok
- But some problems require inequalities or inclusions like
 - $dx/dt \in f(x,t)$ \rightarrow Differential Inclusion! (DI)
- Example: a flywheel with brake torque and applied torque (simple?!)
- Improved model!
- $J d\omega/dt = M_f(\omega) + M_e(t)$ where $M_f = -M_{fmax}$ for $\omega > 0$ and $M_f = M_{fmax}$ for $\omega < 0$ and $-M_{fmax} < M_f < M_{fmax}$ for $\omega = 0$
- This could handle also $\omega = 0$ case, ex. brake sticking
- But now we have a differential inclusion $d\omega/dt \in f(\omega,t)$. It requires special solvers.



MULTIFUNCTION!

ω





Measure Differential Inclusions



- What if the velocity must have discontinuities?
 - ...because of impulses,
 - ..because of impacts,
 - ..because of friction effects such as in Painlevé paradox
- The RHS has 'peaks' (impulses) → measure distributions The velocity has 'jumps' → function of bounded variation
- Measure Differential Inclusion (MDI): strong definition [Moreau]

 $\mathrm{d}\mu/\mathrm{d}\nu(t) \in K(t)$

For singular decomposition of Borel measure $\mu=m\,
u+\mu_s$

$$m(t) \in K(t)$$
 $\frac{\mathrm{d}\mu_s}{\mathrm{d}|\mu_s|}(t) \in K(t)_\infty$

Our DVI model

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- Mechanical system with
 - Set $\mathcal{G}_{\mathcal{B}}$ of bilateral joints
 - Set $\mathcal{G}_{\mathcal{A}}$ of point contacts
 - External forces



$$\begin{split} \dot{\boldsymbol{q}} &= \Gamma(\boldsymbol{q})\boldsymbol{v} \\ M(\boldsymbol{q}) \frac{d\boldsymbol{v}}{dt} &= \sum_{i \in \mathcal{G}_{\mathcal{B}}} \widehat{\gamma}_{\mathcal{B}}^{i} \nabla \Psi^{i} + \sum_{i \in \mathcal{G}_{\mathcal{A}}} \widehat{\gamma}_{\mathcal{A}}^{i} D^{i} + \boldsymbol{f}_{t}(t, \boldsymbol{q}, \boldsymbol{v}) \\ \Psi^{i}(\boldsymbol{q}, t) \in \emptyset, \quad i \in \mathcal{G}_{\mathcal{B}} \\ \widehat{\gamma}_{\mathcal{A}}^{i} \in \mathsf{SOL}\left(\Upsilon^{i}, F(t, \boldsymbol{q}(t), \boldsymbol{v}(t), \cdot)\right), \quad i \in \mathcal{G}_{\mathcal{A}}. \end{split}$$

Bilateral constraint equations Contact forces VIs

Our DVI model

 Do DVI time-step discretization, as a Measure Differential Inclusion MDI

 It leads to a Nonlinear Complementarity Problem (NCP), also a Variational Inequality (VI)

Solve VI at each time step for
unknown speeds
unknown reaction impulses





Cone complementarity



• A modification (relaxation, to get a convex problem):

$$\begin{split} M(\boldsymbol{v}^{(l+1)} - \boldsymbol{v}^{l}) &= \sum_{i \in \mathcal{A}(q^{(l)}, \epsilon)} \left(\gamma_{n}^{i} \boldsymbol{D}_{n}^{i} + \gamma_{u}^{i} \boldsymbol{D}_{u}^{i} + \gamma_{v}^{i} \boldsymbol{D}_{v}^{i} \right) \cdot \\ &+ \sum_{i \in \mathcal{G}_{\mathcal{B}}} \left(\gamma_{b}^{i} \nabla \Psi^{i} \right) + h \boldsymbol{f}_{t}(t^{(l)}, \boldsymbol{q}^{(l)}, \boldsymbol{v}^{(l)}) \\ 0 &= \frac{1}{h} \Psi^{i}(\boldsymbol{q}^{(l)}) + \nabla \Psi^{i^{T}} \boldsymbol{v}^{(l+1)} + \frac{\partial \Psi^{i}}{\partial t}, \quad i \in \mathcal{G}_{\mathcal{B}} \\ 0 &\leq \frac{1}{h} \Phi^{i}(\boldsymbol{q}^{(l)}) + \nabla \Phi^{i^{T}} \boldsymbol{v}^{(l+1)} \boxed{-\mu^{i} \sqrt{(\boldsymbol{D}_{u}^{i,T} \boldsymbol{v})^{2} + (\boldsymbol{D}_{v}^{i,T} \boldsymbol{v})^{2}}} \\ &\perp \quad \gamma_{n}^{i} \geq 0, \; i \in \mathcal{A}(\boldsymbol{q}^{(l)}, \epsilon) \\ \left(\gamma_{u}^{i}, \gamma_{v}^{i} \right) &= \operatorname{argmin}_{\mu^{i} \gamma_{n}^{i} \geq \sqrt{(\gamma_{u}^{i})^{2} + (\gamma_{v}^{i})^{2}}} \quad i \in \mathcal{A}(\boldsymbol{q}^{(l)}, \epsilon) \\ &\left[\boldsymbol{v}^{T}(\gamma_{u} \boldsymbol{D}_{u}^{i} + \gamma_{v} \boldsymbol{D}_{v}^{i}) \right] \\ \boldsymbol{q}^{(l+1)} &= \boldsymbol{q}^{(l)} + h \boldsymbol{v}^{(l+1)}, \end{split}$$

For small h and/or small speeds and/or small friction, almost no differences from the Coulomb theory. Also, convergence proved as in the original scheme.

[see M.Anitescu, "Optimization Based Simulation of Nonsmooth Rigid Body Dynamics"]

Cone complementarity

• Aiming at a more compact formulation:

$$\begin{aligned} \boldsymbol{b}_{\mathcal{A}} &= \left\{ \frac{1}{h} \Phi^{i_{1}}, 0, 0, \frac{1}{h} \Phi^{i_{2}}, 0, 0, \dots, \frac{1}{h} \Phi^{i_{n_{\mathcal{A}}}}, 0, 0 \right\} \\ \boldsymbol{\gamma}_{\mathcal{A}} &= \left\{ \gamma_{n}^{i_{1}}, \gamma_{u}^{i_{1}}, \gamma_{v}^{i_{1}}, \gamma_{n}^{i_{2}}, \gamma_{u}^{i_{2}}, \gamma_{v}^{i_{2}}, \dots, \gamma_{n}^{i_{n_{\mathcal{A}}}}, \gamma_{u}^{i_{n_{\mathcal{A}}}}, \gamma_{v}^{i_{n_{\mathcal{A}}}} \right\} \\ \boldsymbol{b}_{\mathcal{B}} &= \left\{ \frac{1}{h} \Psi^{1} + \frac{\partial \Psi^{1}}{\partial t}, \frac{1}{h} \Psi^{2} + \frac{\partial \Psi^{2}}{\partial t}, \dots, \frac{1}{h} \Psi^{n_{\mathcal{B}}} + \frac{\partial \Psi^{n_{\mathcal{B}}}}{\partial t} \right\} \\ \boldsymbol{\gamma}_{\mathcal{B}} &= \left\{ \gamma_{b}^{1}, \gamma_{b}^{2}, \dots, \gamma_{b}^{n_{\mathcal{B}}} \right\} \\ D_{\mathcal{A}} &= \left[D^{i_{1}} |D^{i_{2}}| \dots |D^{i_{n_{\mathcal{A}}}} \right], \quad i \in \mathcal{A}(\boldsymbol{q}^{l}, \epsilon) \quad D^{i} = \left[\boldsymbol{D}_{n}^{i} |\boldsymbol{D}_{u}^{i}| \boldsymbol{D}_{v}^{i} \right] \\ D_{\mathcal{B}} &= \left[\nabla \Psi^{i_{1}} |\nabla \Psi^{i_{2}}| \dots |\nabla \Psi^{i_{n_{\mathcal{B}}}} \right], \quad i \in \mathcal{G}_{\mathcal{B}} \end{aligned}$$

 $oldsymbol{b}_{\mathcal{E}} \in \mathbb{R}^{n_{\mathcal{E}}} = \{oldsymbol{b}_{\mathcal{A}}, oldsymbol{b}_{\mathcal{B}}\}$

 $oldsymbol{\gamma}_{\mathcal{E}} \in \mathbb{R}^{n_{\mathcal{E}}} = \{oldsymbol{\gamma}_{\mathcal{A}},oldsymbol{\gamma}_{\mathcal{B}}\}$

 $D_{\mathcal{E}} = [D_{\mathcal{A}}|D_{\mathcal{B}}]$



• We also introduce the convex cone

$$\Upsilon = \left(igoplus_{i \in \mathcal{A}(\boldsymbol{q}^l, \epsilon)} \mathcal{FC}^i
ight) igoplus \left(igoplus_{i \in \mathcal{G}_{\mathcal{B}}} \mathcal{BC}^i
ight)$$

• ..and its polar cone:

is *i*-th friction cone

 \mathcal{FC}^i

$$\Upsilon^{\circ} = \left(\bigoplus_{i \in \mathcal{A}(\boldsymbol{q}^{l}, \epsilon)} \mathcal{FC}^{i \circ} \right) \bigoplus \left(\bigoplus_{i \in \mathcal{G}_{\mathcal{B}}} \mathcal{BC}^{i \circ} \right)$$

 \mathcal{BC}^i

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Cone complementarity

• We introduce the Delassus operator N

$$N = D_{\mathcal{E}}^T M^{-1} D_{\mathcal{E}}$$
$$\boldsymbol{r} = D_{\mathcal{E}}^T M^{-1} \tilde{\boldsymbol{k}} + \boldsymbol{b}_{\mathcal{E}} \quad \tilde{\boldsymbol{k}}^{(l)} = M \boldsymbol{v}^{(l)} + h \boldsymbol{f}_{t}(t^{(l)}, \boldsymbol{q}^{(l)}, \boldsymbol{v}^{(l)})$$

• Finally we formulate everything as a Cone Complementarity Problem (CCP):

$$M(v^{(l+1)} - v^{l}) = \sum_{i \in \mathcal{A}(q^{(l)}, e)} (\gamma_{n}^{i} D_{n}^{i} + \gamma_{u}^{i} D_{u}^{i} + \gamma_{v}^{i} D_{v}^{i}) + \sum_{i \in \mathcal{G}_{\mathcal{B}}} (\gamma_{n}^{i} \nabla \Psi^{i}) + hf_{t}(t^{(l)}, q^{(l)}, v^{(l)}) \\ 0 = \frac{1}{h} \Psi^{i}(q^{(l)}) + \nabla \Psi^{i^{T}} v^{(l+1)} + \frac{\partial \Psi^{i}}{\partial t}, i \in \mathcal{G}_{\mathcal{B}} \\ 0 \leq \frac{1}{h} \Phi^{i}(q^{(l)}) + \nabla \Phi^{i^{T}} v^{(l+1)} \\ \perp \gamma_{n}^{i} \geq 0, i \in \mathcal{A}(q^{(l)}, \epsilon) \\ (\gamma_{u}^{i}, \gamma_{v}^{i}) = \underset{u^{i} \gamma_{n}^{i} \geq \sqrt{(\gamma_{v}^{i})^{2} + (\gamma_{v}^{i})^{2}}}{i \in \mathcal{A}(q^{(l)}, \epsilon)} i \in \mathcal{A}(q^{(l)}, \epsilon) \\ [v^{T}(\gamma_{u} D_{u}^{i} + \gamma_{v} D_{v}^{i})] \\ (N \gamma_{\mathcal{E}} + r) \in -\Upsilon^{\circ} \quad \bot \quad \gamma_{\mathcal{E}} \in \Upsilon$$
becomes..



DVI Elasto-Plastic contact

• DVI formulation can be extended to more general friction/contact laws





DVI Elasto-Plastic contact

• DVI formulation can be extended to more general friction/contact laws



DVI advanced contact laws





DVI advanced contact laws







Compliant, plastic cohesion and compression



- In general, DVI are useful for various reasons that are diffult to handle in DAE:
- very stiff or rigid contacts \rightarrow set valued force laws \rightarrow VI
- plasticity in contacts \rightarrow yield surfaces \rightarrow VI
- friction \rightarrow set valued force laws \rightarrow VI



CCP solvers in Chrono

In the DVI-MDI time-stepper, a VI (or CCP) must be solved at each time step.

Which methods are available to solve a CCP in Chrono?

- Fixed-point solvers:
 - Projected-SOR
 - Projected-GaussSeidell
 - Projected-Symmetric-SOR
- Krylov spectral methods
 - Barzilai-Borwein
 - Nesterov Accelerated Projected Gradient Descent (APGD)



P-SOR solver for CCP $(N\gamma_{\mathcal{E}} + r) \in -\Upsilon^{\circ} \perp \gamma_{\mathcal{E}} \in \Upsilon$

• Fixed point iteration with projection on cones:

 $\gamma^{r+1} = \lambda \Pi_{\Upsilon} \left(\gamma^r - \omega B^r \left(N \gamma^r + r + K^r \left(\gamma^{r+1} - \gamma^r \right) \right) \right) + (1 - \lambda) \gamma^r$ *With* $N = D^T M^{-1} D$

At each *r*-th iteration:

$$\int_{\text{Loop on all i-th constraints}} \delta^{i,r+1} = \gamma^{i,r} - \omega \eta_i \left(D^{i,T} M^{-1} \left(\sum_{z=1}^{i-1} D^z \gamma^{z,r+1} + \sum_{z=i}^{n_A} D^z \gamma^{z,r} + \tilde{k}^i \right) + b^i \right)$$



If *i*-th is a scalar bilateral constraint





- •The projection operator must be non-extensive, i.e. lipschitzian with $||f(a)-f(b)|| \le ||a-b||$
- For each frictional contact constraint:

$$\Pi_{\Upsilon} = \left\{ \Pi_{\Upsilon_1}(\gamma_1)^T, \dots \Pi_{\Upsilon_{n_{\mathcal{A}}}}(\gamma^{n_{\mathcal{A}}})^T, \Pi_b^1(\gamma_b^1), \dots, \Pi_b^{n_{\mathcal{B}}}(\gamma_b^{n_{\mathcal{B}}}) \right\}^T$$



•For each bilateral constraint, simply do nothing.

•The complete operator:

$$\forall i \in \mathcal{A}(\boldsymbol{q}^{(l)}, \epsilon)$$

$$\gamma_r < \mu_i \gamma_n \qquad \Pi_i = \gamma_i$$

$$\gamma_r < -\frac{1}{\mu_i} \gamma_n \qquad \Pi_i = \{0, 0, 0\}$$

$$\gamma_r > \mu_i \gamma_n \land \gamma_r > -\frac{1}{\mu_i} \gamma_n \qquad \Pi_{i,n} = \frac{\gamma_r \mu_i + \gamma_n}{\mu_i^2 + 1}$$

$$\Pi_{i,u} = \gamma_u \frac{\mu_i \Pi_{i,n}}{\gamma_r}$$

$$\Pi_{i,v} = \gamma_v \frac{\mu_i \Pi_{i,n}}{\gamma_r}$$



• P-SOR in incremental efficient form

$$\begin{split} \delta^{i,r+1} &= \gamma^{i,r} - \omega \eta_i \left(D^{i,T} M^{-1} \left(\sum_{z=1}^{i-1} D^z \gamma^{z,r+1} + \sum_{z=i}^{n_{\mathcal{A}}} D^z \gamma^{z,r} + \tilde{k}^i \right) + b^i \right) \\ \gamma^{i,r+1} &= \lambda \Pi_{\Upsilon^i} \left(\delta^{i,r+1} \right) + (1-\lambda) \gamma^{i,r} \end{split}$$

$$\begin{aligned} & \text{Avoid these loops, each iteration would only one of these norms} \end{aligned}$$

Avoid these loops, otherwise each iteration would be $O(n^2)$ Only one of these multiplier changes at each iteration...

We know that: $\boldsymbol{v} = M^{-1}D \ \boldsymbol{\gamma} + M^{-1} \tilde{\boldsymbol{k}}$...so we rewrite:

$$\begin{cases} \boldsymbol{\delta}^{i.r+1} = \left(\boldsymbol{\gamma}^{i.r} - \omega \boldsymbol{\eta}^{i} \left(D^{i,T} \boldsymbol{v}^{r} + \boldsymbol{b}^{i} \right) \right); \\ \boldsymbol{\gamma}^{i.r+1} = \lambda \Pi_{\Upsilon} \left(\boldsymbol{\delta}^{i.r+1} \right) + (1-\lambda) \boldsymbol{\gamma}^{i.r}; \\ \Delta \boldsymbol{\gamma}^{i.r+1} = \boldsymbol{\gamma}^{i.r+1} - \boldsymbol{\gamma}^{i.r}; \\ \boldsymbol{v} := \boldsymbol{v} + M^{-1} D^{i} \Delta \boldsymbol{\gamma}^{i.r+1} \end{cases}$$

Loop on all i-th constraints



• Pseudocode

(1)	// Pre-compute some data for friction constraints
(2)	for $i := 1$ to $n_{\mathcal{A}}$
(3)	$s_a^i = M^{-1}D^i$
(4)	$g_a^i = D^{i,T} \boldsymbol{s}_a^i$
(5)	$\eta_a^i = \frac{3}{\operatorname{Trace}(q_a^i)}$
(6)	// Pre-compute some data for bilateral constraints
(7)	for $i := 1$ to $n_{\mathcal{B}}$
(8)	$s_b^i = M^{-1} \nabla \Psi^i$
(9)	$g_b^i = \boldsymbol{ abla} \Psi^{i,T} s_b^i$
(10)	$\eta_b^i = rac{1}{g_b^i}$
(11)	0
(12)	// Initialize impulses
(13)	if warm start with initial guess $\gamma^*_{\mathcal{E}}$
(14)	$oldsymbol{\gamma}^0_{\mathcal{E}} = oldsymbol{\gamma}^*_{\mathcal{E}}$
(15)	else
(16)	$\gamma^0_{\mathcal{E}}=0$
(17)	
(18)	// Initialize speeds
(19)	$\boldsymbol{v} = \sum_{i=1}^{n_{\mathcal{A}}} \boldsymbol{s}_{a}^{i} \boldsymbol{\gamma}_{a}^{i,0} + \sum_{i=1}^{n_{\mathcal{B}}} s_{b}^{i} \boldsymbol{\gamma}_{b}^{i,0} + M^{-1} \tilde{\boldsymbol{k}}$

(21)	// Main iteration loop
(22)	for $r := 0$ to r_{max}
(23)	// Loop on frictional constraints
(24)	for $i := 1$ to $n_{\mathcal{A}}$
(25)	$\boldsymbol{\delta}_{a}^{i,r} = \left(\boldsymbol{\gamma}_{a}^{i,r} - \omega \eta_{a}^{i} \left(D^{i,T} \boldsymbol{v}^{r} + \boldsymbol{b}_{a}^{i} \right) \right);$
(26)	$\boldsymbol{\gamma}_{a}^{i,r+1} = \lambda \Pi_{\Upsilon} \left(\boldsymbol{\delta}_{a}^{i,r} \right) + (1-\lambda) \boldsymbol{\gamma}_{a}^{i,r} ;$
(27)	$\Delta oldsymbol{\gamma}_a^{i,r+1} = oldsymbol{\gamma}_a^{i,r+1} - oldsymbol{\gamma}_a^{i,r}$;
(28)	$oldsymbol{v}:=oldsymbol{v}+oldsymbol{s}_a^{i^{T}}\Deltaoldsymbol{\gamma}_a^{i,r+1}.$
(29)	// Loop on bilateral constraints
(30)	for $i := 1$ to $n_{\mathcal{B}}$
(31)	$\delta_b^{i,r} = \left(\gamma_b^{i,r} - \omega \eta_b^i \left(\nabla \boldsymbol{\Psi}^{i,T} \boldsymbol{v}^r + b_b^i\right)\right);$
(32)	$\gamma_b^{i,r+1} = \lambda \Pi_{\Upsilon} \left(\delta_b^{i,r} \right) + (1-\lambda) \gamma_b^{i,r} ;$
(33)	$\Delta \gamma_b^{i,r+1} = \gamma_b^{i,r+1} - \gamma_b^{i,r} ;$
(34)	$oldsymbol{v} := oldsymbol{v} + s_b^{i^T} \Delta \gamma_b^{i,r+1}.$
(35)	, i i i i i i i i i i i i i i i i i i i
(36)	$\operatorname{return} oldsymbol{\gamma}_{\mathcal{E}}, oldsymbol{v}$



- Very robust algorithm
- It supports redundant constraints
- It is very fast good for robotics, etc.
- ...but it has slow convergence:



• Other methods, without the convergence stall, are needed when high precision is needed



• Use SetSolverType() to change the solver:

// change the solver to P-SOR:
my_system.SetSolverType(ChSystem::SOLVER_SOR);

// use high iteration number if constraints tend to 'dismount' or contacts interpenetrate:
my_system.SetMaxItersSolverSpeed(90);



• In case of convexified problem (i.e. 'associative flows' as our CCP) one can express the VI as a constrained quadratic program:

min
$$f(\mathbf{x}) = \frac{1}{2}\mathbf{x}^T A \mathbf{x} + \mathbf{x}^T \mathbf{b}$$

s.t. $\mathbf{x} \in \mathscr{K}$

- One can use the Spectral Projected Gradient (SPG) method for solving it!
- It is a modified Barzilai-Borwein iteration

• Our modified P-SPG-FB algorithm

- Supports premature termination with fall-back strategy (FB)
- Uses alternating step sizes
- Uses diagonal preconditioning (with isothropic cone scaling)

$$P = \overline{\operatorname{diag}}(A)$$

• Performs projection onto Lorentz cones

ALGORITHM P-SPG-FB(
$$\mathcal{A}$$
, b, \mathbf{x}_0 ,
 \mathscr{K} , $P \mapsto \mathbf{x}$)
 $\mathbf{x}_0 := \Pi_{\mathscr{K}}(\mathbf{x}_0)$, $\mathbf{x}_{FB} = \mathbf{x}_0$,
 $\hat{\alpha}_0 \in [\alpha_{min}, \alpha_{max}]$
 $\mathbf{g}_0 := A\mathbf{x}_0 + \mathbf{b}$, $f(\mathbf{x}_0) = \frac{1}{2}\mathbf{x}_0^T A\mathbf{x}_0 + \mathbf{x}_0^T \mathbf{b}$, $w_0 = 10^{29}$
for $j := 0$ to N_{max}
 $\mathbf{p}_j = P^{-1}\mathbf{g}_j$
 $\mathbf{d}_j = \Pi_{\mathscr{K}}(\mathbf{x}_j - \hat{\alpha}_j\mathbf{p}_j) - \mathbf{x}_j$
if $\langle \mathbf{d}_j, \mathbf{g}_j \rangle \ge 0$
 $\mathbf{d}_j = \Pi_{\mathscr{K}}(\mathbf{x}_j - \hat{\alpha}_j\mathbf{g}_j) - \mathbf{x}_j$
 $\lambda := 1$
while line search
 $\mathbf{x}_{j+1} := \mathbf{x}_j + \lambda \mathbf{d}_j$
 $\mathbf{g}_{j+1} := A\mathbf{x}_{j+1} + \mathbf{b}$
 $f(\mathbf{x}_{j+1}) = \frac{1}{2}\mathbf{x}_j^T A\mathbf{x}_{j+1} + \mathbf{x}_{j+1}^T \mathbf{b}$
if $f(\mathbf{x}_{j+1}) > \max_{i=0,\dots,\min(j,N_{GLL})} f(\mathbf{x}_{j-i}) + \gamma \lambda \langle \mathbf{d}_j, \mathbf{g}_j \rangle$
 $define \lambda_{new} \in [\sigma_{\min}\lambda, \sigma_{\max}\lambda]$ and
repeat line search
else
terminate line search
 \mathbf{else}
 $\mathbf{terminate line search}$
 $\hat{\mathbf{s}}_j = \mathbf{x}_{j+1} - \mathbf{x}_j$
 $\mathbf{y}_j = \mathbf{g}_{j+1} - \mathbf{g}_j$
if j is odd
 $\hat{\alpha}_{j+1} = \frac{\langle \mathbf{s}_j, \mathbf{y}_j \rangle}{\langle \mathbf{s}_j, \mathbf{y}_j \rangle}$
 $\hat{\mathbf{a}}_{j+1} = \min(\alpha_{\max}, \max(\alpha_{\min}, \hat{\alpha}_{j+1})))$
 $w_{j+1} = ||[\mathbf{x}_{j+1} - \Pi_{\mathscr{K}}(\mathbf{x}_{j+1} - \tau_g \mathbf{g}_{j+1})] / \tau_g||_2$
 $= ||\varepsilon||_2$
if $w_{j+1} \leq \min_{k=0,\dots,j} w_k$
 $\mathbf{x}_{FB} = \mathbf{x}_{j+1}$





- Comparison with other Krylov solvers for simple linear case
- (only bilateral constraints):









- Comparison with other solvers for complemetarity problems
- (only unilateral contacts, no friction)







- Comparison with other solvers for complemetarity problems
- (unilateral contacts AND friction few solvers can handle it)





• Effect of preconditioning:







• Use SetSolverType() to change the solver:

// change the solver to Barzilai-Borwein P-SPG-FB:
my_system.SetSolverType(ChSystem::SOLVER_BARZILAIBORWEIN);

// will terminate iterations when this tolerance is reached:
my_system.SetTolForce(1e-7);

// use high iteration number if constraints tend to 'dismount' or contacts interpenetrate:
my_system.SetMaxItersSolverSpeed(110);



APGD solver for CCP

- Draws on the Nesterov's Accelerated Projected Gradient Descend
- It operates as a non-linear optimization for:

min
$$f(\mathbf{x}) = \frac{1}{2}\mathbf{x}^T A \mathbf{x} + \mathbf{x}^T \mathbf{b}$$

s.t. $\mathbf{x} \in \mathscr{K}$

• Properties of convergence are very similar to P-SPG-FB just presented.



APGD solver for CCP

• Use SetSolverType() to change the solver:

// change the solver to Nesterov' APGD:
my_system.SetSolverType(ChSystem::SOLVER_APGD);

// will terminate iterations when this tolerance is reached:
my_system.SetTolForce(1e-7);

// use high iteration number if constraints tend to 'dismount' or contacts interpenetrate:
my_system.SetMaxItersSolverSpeed(110);

Time-integration & solvers cheat-sheet



	<u>ح ک</u>								Time integrator compatibility	
	LINEA	FEA* (DAE)	CCP	FEA* (DVI)	lterative	Redundant constraints	Optional Chrono module	Large systems	ннт	EULER_IMPLICI T_LINEARIZED
SOR		*	••	*		••		•••	2	O O O DAE, DVI
BARZILAIBORWEIN		*	•••	*		••		•••	● DAE	O O O DAE, DVI
APGD		*	•••	*		••		•••	• DAE	●●● DAE, DVI
MINRES		•1		*		•••		•••	● ● DAE	• DAE
MKL		•••		*				••	OAE	• DAE
MUMPS		•••		*		•		••	●●● DAE	DAE

* For FEA, the solver must support stiffness and damping matrices. Note that FEA in NSC is not yet possible at the moment.

1 The MINRES solver might converge too slow when using finite elements with ill-conditioned stiffness

2 The SOR solver is not precise enough for good HHT convergence, except for simple systems